# ME451 Kinematics and Dynamics of Machine Systems

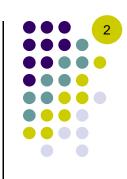
#### Introduction to Dynamics

6.1

November 11, 2014

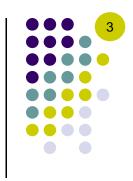


#### Before we get started...



- Last time (before the exam)
  - Started working towards deriving the equations of motion of a rigid body
- Today
  - Wrap up the Newton-Euler equations of motion for a rigid body
  - Properties of the Centroid and Mass Moment of Inertia, Inertial Properties of Composite Bodies
- Project 1 Due date: Nov 18 at 11:59 PM
  - Requires you to use simEngine2D in conjunction with excavator example discussed in class
  - Not trivial, requires some thinking
- HW due on Th includes ADAMS, MATLAB, pen-and-paper
  - Probably the toughest assignment this semester

#### Midterm Exam 1



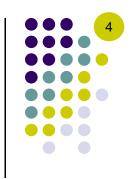
Highest score: 100

Average: 85

Standard Deviation: 16.88

- Problem A: KDOF question caused lots of problems
- Problem B: Two different ways of modeling the same mechanism
  - Scores not as high as I was hoping
  - People not reading what was asked (provided the equations as well)
- Problem 3: overall, good understanding of how to pose the set of position, velocity, and acceleration constraint equations
  - People seem to have understood Newton-Raphson

### D'Alembert's Principle



For **consistent** virtual displacements  $\delta \mathbf{r}^P$ 

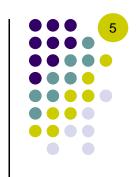
$$\int_{m} (\delta \mathbf{r}^{P})^{T} \ddot{\mathbf{r}}^{P} dm(P) = \int_{m} (\delta \mathbf{r}^{P})^{T} \mathbf{f}_{d}(P) dm(P)$$

This is D'Alembert's principle for the motion of a rigid body. D'Alemebert's principle is an extension of the *Principle of Virtual Work* to the case of accelerated motion.



Jean-Baptiste d'Alembert (1717–1783)

## Virtual Displacements in terms of Variations in Generalized Coordinates (1/2) Virtual Displacements in terms of



We have concluded that the following:

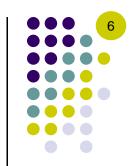
$$\int_m (\delta \mathbf{r}^P)^T \ddot{\mathbf{r}}^P dm(P) = \int_m (\delta \mathbf{r}^P)^T \mathbf{f}_d(P) dm(P)$$

must hold for all virtual displacements  $\delta \mathbf{r}^P$  that are consistent with the constraints imposing rigid-body motion.

Next Step: Express the virtual displacements  $\delta \mathbf{r}^P$  using variations in the generalized coordinates q

• In this step we keep in mind that  $\delta \mathbf{r}^P$  must be **consistent** with the rigidbody virtual displacement, that is, we are dealing with a rigid body here

# Virtual Displacements in terms of Variations in Generalized Coordinates (2/2)



Recall that

$$\delta \mathbf{r}^P = \delta \mathbf{r} + \delta \phi \mathbf{B} \mathbf{s'}^P \quad \text{and} \quad \ddot{\mathbf{r}}^P = \ddot{\mathbf{r}} + \ddot{\phi} \mathbf{B} \mathbf{s'}^P - \dot{\phi}^2 \mathbf{A} \mathbf{s'}^P$$

Use these relations to expand

$$\int_m (\delta \mathbf{r}^P)^T \ddot{\mathbf{r}}^P dm(P) = \int_m (\delta \mathbf{r}^P)^T \mathbf{f}_d(P) dm(P)$$

(which only holds for **consistent**  $\delta \mathbf{r}^P$ ) to

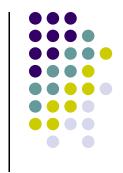
$$\delta \mathbf{r}^{T} \ddot{\mathbf{r}} \int_{m} dm(P) + \left( \delta \mathbf{r}^{T} (\ddot{\phi} \mathbf{B} - \dot{\phi}^{2} \mathbf{A}) + \delta \phi \ddot{\mathbf{r}}^{T} \mathbf{B} \right) \int_{m} \mathbf{s'}^{P} dm(P)$$

$$+ \delta \phi \int_{m} (\mathbf{s'}^{P})^{T} \mathbf{B}^{T} (\ddot{\phi} \mathbf{B} - \dot{\phi}^{2} \mathbf{A}) \mathbf{s'}^{P} dm(P)$$

$$= \delta \mathbf{r}^{T} \int_{m} \mathbf{f}_{d}(P) dm(P) + \delta \phi \int_{m} (\mathbf{s'}^{P})^{T} \mathbf{B}^{T} \mathbf{f}_{d}(P) dm(P)$$

(which holds for **arbitrary** variations  $\delta \mathbf{r}$  and  $\delta \phi !)$ 

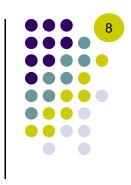




6.1.2, 6.1.3

### Variational EOM with Centroidal Coordinates Newton-Euler Differential EOM

#### **Centroidal Reference Frames**



- The variational EOM for a single rigid body can be significantly simplified if we pick a special LRF
- A centroidal reference frame is an LRF located at the center of mass
- How is such an LRF special?

By definition of the center of mass (more on this later) is the point where the following integral vanishes:

$$\int_{m} \mathbf{s'}^{P} dm(P) = 0$$

#### Variational EOM with Centroidal LRF (1/3)

$$\begin{split} \delta \mathbf{r}^T \ddot{\mathbf{r}} \int_m dm(P) + \left( \delta \mathbf{r}^T (\ddot{\phi} \mathbf{B} - \dot{\phi}^2 \mathbf{A}) + \delta \phi \ddot{\mathbf{r}}^T \mathbf{B} \right) \int_m \mathbf{s'}^P dm(P) \\ + \delta \phi \int_m (\mathbf{s'}^P)^T \mathbf{B}^T (\ddot{\phi} \mathbf{B} - \dot{\phi}^2 \mathbf{A}) \mathbf{s'}^P dm(P) \\ = \delta \mathbf{r}^T \int_m \mathbf{f}_d(P) dm(P) + \delta \phi \int_m (\mathbf{s'}^P)^T \mathbf{B}^T \mathbf{f}_d(P) dm(P) \end{split}$$

• Total body mass:

$$\int_m dm(P) = m$$

• Definition of centroid:

$$\int_{m} \mathbf{s'}^{P} dm(P) = \mathbf{0}$$

$$LHS = m \ \delta \mathbf{r}^T \ \ddot{\mathbf{r}} + J' \ \delta \phi \ \ddot{\phi}$$

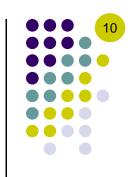
• Definition of mass moment of inertia:

$$\int_{m} (\mathbf{s'}^{P})^{T} \mathbf{B}^{T} \mathbf{B} \mathbf{s'}^{P} \ddot{\phi} dm(P) = \ddot{\phi} \int_{m} (\mathbf{s'}^{P})^{T} \mathbf{s'}^{P} dm(P)$$
$$J' \triangleq \int_{m} (\mathbf{s'}^{P})^{T} \mathbf{s'}^{P} dm(P)$$

• Direct expansion:

$$\int_{m} (\mathbf{s'}^{P})^{T} \mathbf{B}^{T} \mathbf{A} \mathbf{s'}^{P} dm(P) = 0$$

#### Variational EOM with Centroidal LRF (2/3)



$$\begin{split} \delta \mathbf{r}^T \ddot{\mathbf{r}} \int_m dm(P) + \left( \delta \mathbf{r}^T (\ddot{\phi} \mathbf{B} - \dot{\phi}^2 \mathbf{A}) + \delta \phi \ddot{\mathbf{r}}^T \mathbf{B} \right) \int_m \mathbf{s'}^P dm(P) \\ + \delta \phi \int_m (\mathbf{s'}^P)^T \mathbf{B}^T (\ddot{\phi} \mathbf{B} - \dot{\phi}^2 \mathbf{A}) \mathbf{s'}^P dm(P) \\ = \delta \mathbf{r}^T \int_m \mathbf{f}_d(P) dm(P) + \delta \phi \int_m (\mathbf{s'}^P)^T \mathbf{B}^T \mathbf{f}_d(P) dm(P) \end{split}$$

• Resultant of all forces acting on the body:

$$\mathbf{F} = \int_{m} \mathbf{f}_{d}(P) dm(P)$$

• Moment of all forces acting on the body (about the COM):

$$n = \int_{m} (\mathbf{s'}^{P})^{T} \mathbf{B}^{T} \mathbf{f}_{d}(P) dm(P)$$

$$RHS = \delta \mathbf{r}^T \mathbf{F} + \delta \phi \ n$$

## **EOM** for a Single Rigid Body: Newton-Euler Equations



 The variational EOM of a rigid body with a centroidal body-fixed reference frame were obtained as:

$$\delta \mathbf{r}^T \left( m\ddot{\mathbf{r}} - \mathbf{F} 
ight) + \delta \phi \left( J'\ddot{\phi} - n 
ight) = 0 \quad \Leftrightarrow \quad \left[ \delta \mathbf{r}^T \quad \delta \phi 
ight] \left[ egin{matrix} m\ddot{\mathbf{r}} - \mathbf{F} \ J'\ddot{\phi} - n \end{matrix} 
ight] = 0$$

- Assume all forces acting on the body have been accounted for.
- Since  $\delta \mathbf{r}$  and  $\delta \phi$  are arbitrary, using the orthogonality theorem, we get:

$$egin{bmatrix} m\ddot{\mathbf{r}}-\mathbf{F} \ J'\ddot{\phi}-n \end{bmatrix} = \mathbf{0} \quad \Leftrightarrow \quad egin{matrix} m\ddot{\mathbf{r}}=\mathbf{F} \ J'\ddot{\phi}=n \end{cases}$$

- Important: The Newton-Euler equations are valid only if all force effects have been accounted for
  - This includes both applied forces/torques and constraint forces/torques (from interactions with <u>other</u> bodies).

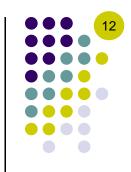


Isaac Newton (1642 – 1727)



Leonhard Euler (1707 – 1783)

#### **Newton-Euler EOM**

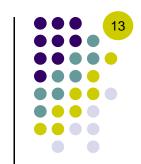


Here's where we are: the EOM for a centroidal LRF (CLRF)

$$egin{bmatrix} m{m}\ddot{\mathbf{r}} - \mathbf{F} \ J'\ddot{\phi} - n \end{bmatrix} = \mathbf{0} \quad \Leftrightarrow \quad m{m}\ddot{\mathbf{r}} = \mathbf{F} \ J'\ddot{\phi} = n \ \end{pmatrix}$$

- Got these second order differential equations starting from "first principles"
  - Newton's laws for a particle
  - The rigid body assumption
- They tell us what the acceleration of the CLRF slapped on the body looks like
  - Recall that this is what we were after: figuring out what the acceleration is
    - Integrate once to get velocity
    - Integrate once again to get positions
    - (easier said than done)

#### Variational EOM with Centroidal LRF (3/3)



Why do we say that the quantity  $\int_m (\mathbf{s'}^P)^T \mathbf{B}^T \mathbf{f}_d(P) dm(P)$  is the *torque* (or *moment*) n of the forces acting on the body?

Consider a force  $\vec{F}$  acting on the body at point P which is located by the vector  $\vec{s}$ . Then, the torque of this force about an axis perpendicular to the x-y plane and passing through the origin of the LRF has magnitude equal to:

$$n = \|\vec{s} \times \vec{F}\|$$

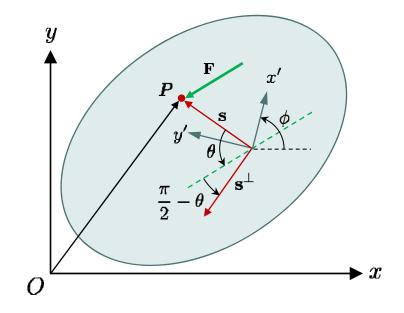
$$= \|\vec{s}\| \cdot \|\vec{F}\| \cdot \sin \theta$$

$$= \|\vec{s}\| \cdot \|\vec{F}\| \cdot \cos \left(\frac{\pi}{2} - \theta\right)$$

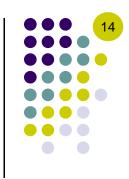
$$= \vec{s}^{\perp} \cdot \vec{F}$$

Using algebraic vectors, we get

$$n = (\mathbf{s}^{\perp})^T \mathbf{F} = (\mathbf{R}\mathbf{s})^T \mathbf{F}$$
  
=  $(\mathbf{R}\mathbf{A}\mathbf{s}')^T \mathbf{F} = (\mathbf{B}\mathbf{s}')^T \mathbf{F}$ 



#### **Roadmap: Check Progress**



What have we done so far?

Derived the variational and differential EOM for a single rigid body

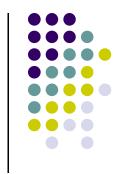
$$egin{bmatrix} m\ddot{\mathbf{r}}-\mathbf{F} \ J'\ddot{\phi}-n \end{bmatrix} = \mathbf{0} \quad \Leftrightarrow \quad m\ddot{\mathbf{r}}=\mathbf{F} \ J'\ddot{\phi}=n \ \end{pmatrix}$$

#### What is left?

Properties of the mass moment of inertia



- Define a general strategy for including external forces in F above
- Treatment of constraint forces
- Derive the variational and differential EOM for systems of constrained bodies



6.1.4, 6.1.5

#### **Properties of the Centroid and Mass Moment of Inertia Inertial Properties of Composite Bodies**

#### Location of the Center of Mass (1/2)



 The center of mass is the point on the body where the weighted relative position of the distributed mass sums to zero:

$$\int_m {\bf s'}^P dm(P) = 0$$

• Question: How can we calculate the location  $\rho''$  of the COM with respect to an LRF O''x''y''?

$$\mathbf{0} = \int_{m} \mathbf{s'}^{P} dm(P)$$

$$= \int_{m} \left( \mathbf{s''}^{P} - \rho'' \right) dm(P)$$

$$= \int_{m} \mathbf{s''}^{P} dm(P) - m\rho''$$

where we have defined the total body mass as:

$$m=\int_m dm(P)$$
  $ho''=rac{1}{m}\int_m {f s''}^P dm(P)$ 

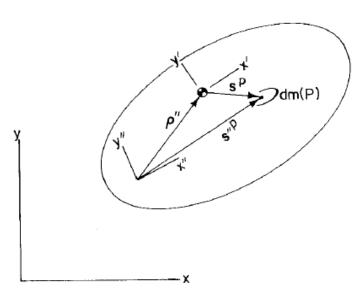


Figure 6.1.3 Location of a centroid.

#### **Location of the Center of Mass (2/2)**

- For a rigid body, the COM is fixed with respect to the body
- If the body has constant density, the COM coincides with the centroid of the body shape
- If the rigid body has a line of symmetry, then the COM is somewhere along that axis

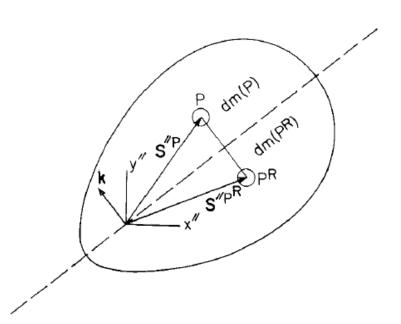


Figure 6.1.4 Body with axis of symmetry.

#### Notes:

- Here, symmetry axis means that both mass distribution and geometry are symmetric with respect to that axis
- If the rigid body has two axes of symmetry, the centroid is on each of them, and therefore is at their intersection

