ME451 Kinematics and Dynamics of Machine Systems

Dynamics of Planar Systems

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Chapter 6



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Before we get started...

• Last Time

- Midterm exam
- Prior to exam: closed the book on the Kinematics Analysis

• Today

- Start Chapter 6: Dynamics
 - Work on Sections 6.1.1 and 6.1.2
- Due Tuesday:
 - Take home exam
 - MATLAB Assignment
 - ADAMS Assignment
- Not much traffic on the forum...

Purpose of Chapter 6



- At the end of this chapter you should understand what "dynamics" means and how you should go about carrying out a dynamics analysis
- We'll learn a couple of things:
 - How to formulate the equations that govern the time evolution of a system of bodies in planar motion
 - These equations are differential equations and they are called equations of motion
 - As many bodies as you wish, connected by any joints we've learned about...
 - How to compute the reaction forces in any joint connecting any two bodies in the mechanism
 - Understand how to properly handle the applied (external) forces to correctly use them in formulating the equations of motion

The Idea, in a Nutshell...



- First part of the class: **Kinematics**
 - You have as <u>many</u> constraints (kinematic and driving) as generalized coordinates
 - <u>No spare</u> degrees of freedom left
 - Position, velocity, acceleration found as the solution of algebraic problems (both nonlinear and linear)
 - We do not care whatsoever about forces applied to the system, we are told what the motions are and that's enough for the purpose of kinematics

• Second part of the class: **Dynamics**

- You only have a few constraints imposed on the system
- You have <u>extra</u> degrees of freedom
- The system evolves in time as a result of external forces applied on it
- We very much care about forces applied and inertia properties of the components of the mechanism (mass, mass moment of inertia)

Some clarifications



- Dynamics **key** question: how can I get the acceleration of each body of the mechanism?
 - Why is acceleration so relevant? If you know the acceleration you can integrate it twice to get velocity and position information for each body
 - How is the acceleration of a body "*i*" measured in the first place?
 - You attach a reference frame on body "*i*" and measure the acceleration of the body reference frame with respect to the global reference frame:

$$\mathbf{\ddot{q}}_i = \left[egin{array}{c} \ddot{x}_i \ \ddot{y}_i \ \ddot{\phi}_i \end{array}
ight.$$

- The answer to the key question: To get the acceleration of each body, you first need to formulate the equations of motion
 - Remember **F=ma**?
 - Actually, the proper way to state this is **ma=F**, which is the "equation of motion", that is, what we are after here

Equations of motion of ONE planar RIGID body



- Framework:
 - We are dealing with <u>rigid</u> bodies
 - For this lecture, we'll consider only one body
 - We'll extend to more bodies next week...
- What are we after?
 - Proving that for one body with a reference frame attached at its center of mass location the equations of motion are:

 $m\ddot{\mathbf{r}} - \mathbf{F} = \mathbf{0}$ Equations of Motion governing translation $J'\ddot{\phi} - n = 0$ Equation of Motion governing rotation

r is the position of the body local reference frame ϕ is the orientation of the body local reference frame

Equations of Motion (EOM) Some clarifications...



- Centroidal reference frame of a body
 - A reference frame located right at the center of mass of that body
 - How is this special? It's special since a certain integral vanishes...

$$\int_{m} \mathbf{s}'^{P} \, d\mathbf{m}(P) = 0$$

- What is J'?
 - Mass moment of inertia

$$J' = \int_{m} \left[\mathbf{s}'^{P} \right]^{T} \mathbf{s}'^{P} d\mathbf{m}(P)$$

NOTE: Textbook uses misleading notation

$$\mathbf{s}'^{PT} \Leftrightarrow \left[\mathbf{s}'^{P}\right]^{T}$$

Two Principles

- Principle of Virtual Work
 - Applies to a collection of particles
 - States that a configuration is an equilibrium configuration if and only if the virtual work of the forces acting on the collection of particle is zero

$$\sum_{i} \delta \mathbf{r}_{i}^{T} \cdot \mathbf{F}_{i} = 0$$

- D'Alembert's Principle
 - For a collection of particles <u>moving</u> around you can still fall back on the Principle of Virtual Work when you also include in the set of forces acting on each particle *i* its inertia force

$$\sum_{i} \delta \mathbf{r}_{i}^{T} \cdot (\mathbf{F}_{i} - m_{i} \ddot{\mathbf{r}}_{i}) = 0$$

- Note: we are talking here about a collection of *particles*
 - Consequently, we'll have to regard each rigid body as a collection of particles that are rigidly connected to each other and that together make up the body



Virtual Displacement and Virtual Work



• Imagine that force $\vec{\mathbf{F}}^P$ acts on a rigid body at point *P*. The virtual work done by this force is

$$\delta W^{F_P} = \left[\delta \mathbf{r}^P\right]^T \cdot \mathbf{F}^P$$

• Here $\delta \mathbf{r}^P$ represents a virtual displacement of the point P in response to a virtual translation and a virtual rotation experienced by the body to which P is attached.



[Small Detour, 3 slides] The Variation $\delta \mathbf{u}$ of a Function $\mathbf{u}(\mathbf{q}, t)$ due to a *small* change in its argument $\mathbf{q} \rightarrow \mathbf{q} + \delta \mathbf{q}$

- Framework: assume you have a vector quantity that depends on \mathbf{q} . Assume that the value of \mathbf{q} changes to $\mathbf{q} + \delta \mathbf{q}$. What is the variation in the quantity that depends on \mathbf{q} due to the said change?
- Specifically, assume the vector quantity of interest is **u**, and **u** depends on **q** and possibly time t:

$$\mathbf{u} = \mathbf{u}(\mathbf{q}, t)$$

• I am interested at a fixed time t in the $\delta \mathbf{u}$ below given \mathbf{q} , $\delta \mathbf{q}$, and the expression of $\mathbf{u}(\mathbf{q})$:

$$\mathbf{q} \longrightarrow \mathbf{u}(\mathbf{q},t) \qquad \mathbf{q} + \delta \mathbf{q} \longrightarrow \mathbf{u}(\mathbf{q} + \delta \mathbf{q},t) = \mathbf{u}(\mathbf{q},t) + \mathbf{\delta u}$$

$$\delta \mathbf{u} = ?$$





$$\delta \mathbf{u} = ?$$



• Without getting into details (more on this in ME751 or in a Calculus of Variations class/textbook)

 $\delta \mathbf{u} = \mathbf{u}_{\mathbf{q}} \cdot \delta \mathbf{q}$

• Likewise, given two functions $\mathbf{f}(\mathbf{q}, t)$ and $\mathbf{g}(\mathbf{q}, t)$, we have that

$$\delta(\mathbf{f} + \mathbf{g}) = \delta \mathbf{f} + \delta \mathbf{q} \qquad \qquad \delta(\mathbf{f} - \mathbf{g}) = \delta \mathbf{f} - \delta \mathbf{q}$$

[Example] Calculus of Variations

 Indicate the change in the quantities below that are a consequence of applying a virtual displacement δq to the generalized coordinates q

Assumptions: $\mathbf{g} = \mathbf{g}(\mathbf{q})$ $\mathbf{p} = \mathbf{p}(\mathbf{q})$ \mathbf{C} - constant matrix

 $\mathbf{h}(\mathbf{q}) = \mathbf{C}\mathbf{q}$

$$h(\mathbf{q}) = \mathbf{g}^T \mathbf{p}$$

$$h(\mathbf{q}) = \mathbf{p}^T \mathbf{C} \mathbf{q}$$

The dimensions of the vectors and matrix above such that all the operations listed can be carried out. 12

Calculus of Variations in ME451

- In our case we are interested in variations of kinematic quantities (locations of a point P, of A matrix, etc.) due to a variations in the location and orientation of a body.
- Variation in location of the L-RF:

$$\mathbf{r} \longrightarrow \mathbf{r} + \delta \mathbf{r}$$

• Variation in orientation of the L-RF:

$$\phi \longrightarrow \phi + \delta \phi$$

 As far as the change of orientation matrix A(φ) is concerned, using the result stated two slides ago, we have that a variation in the orientation leads to the following variation in A:

$$\delta {f A} = {d {f A} \over d \phi} \; \delta \phi = {f B} \; \delta \phi$$



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Calculus of Variations in ME451 Virtual Displacement of a Point P Attached to a Body

- Original position of *P*:
- Position of P after the small change in the position and orientation of the rigid body:

$$\mathbf{r}^{P} + \delta \mathbf{r}^{P} = (\mathbf{r} + \delta \mathbf{r}) + (\mathbf{A} + \delta \mathbf{A})\bar{\mathbf{s}}^{P}$$

 $\mathbf{r}^P = \mathbf{r} + \mathbf{A}\bar{\mathbf{s}}^P$

• Net change in position of point *P*:

$$\delta \mathbf{r}^{P} = (\mathbf{r}^{P} + \delta \mathbf{r}^{P}) - \mathbf{r}^{P} = \delta \mathbf{r} + \delta \mathbf{A} \ \bar{\mathbf{s}}^{P} = \delta \mathbf{r} + \mathbf{B} \ \bar{\mathbf{s}}^{P} \delta \phi$$
Location, after Location,

• Matrix-Vector Form:

Location, after Location Virtual Displacement Original

$$\delta \mathbf{r}^P = \begin{bmatrix} \mathbf{I}_{2 \times 2} & , & \mathbf{B} \ \bar{\mathbf{s}}^P \end{bmatrix} \cdot \begin{bmatrix} \delta \mathbf{r} \\ \delta \phi \end{bmatrix}$$





Deriving the EOM

Some Clarifications



- Assumptions:
 - All bodies that we work with are rigid^{*}
 - The bodies undergo planar motion
- Start from scratch, that is, from the dynamics of a material point, work our way up to a body, then to a collection of bodies that are interacting through kinematic joints and/or friction & contact
- Derivation that follows next is also in the textbook

Some Clarifications

[regarding the "Rigid Body" concept]



• **Remark 1**: For a rigid body, the distance between two internal points P and R of the body does not change in time:

$$(\mathbf{r}^P - \mathbf{r}^R)^T \cdot (\mathbf{r}^P - \mathbf{r}^R) = \text{const.}$$

- Then,

$$(\mathbf{r}^P - \mathbf{r}^R)^T \cdot \delta(\mathbf{r}^P - \mathbf{r}^R) = 0$$

• Remark 2: For a rigid body, any internal force f(P, R) acting between points P and R is along the direction defined by these two points. That is, with k a scalar that might depend on time,

$$\mathbf{f}(P,R) = k(\mathbf{r}^P - \mathbf{r}^R)$$

• Based on the previous two equations, one can conclude that

$$\mathbf{f}^{T}(P,R) \cdot \delta(\mathbf{r}^{P} - \mathbf{r}^{R}) = \left[\delta(\mathbf{r}^{P} - \mathbf{r}^{R})\right]^{T} \cdot \mathbf{f}(P,R) = 0$$

• In plain English, the virtual work of the internal forces is zero. We'll revisit/need this shortly.

Road Map [2 weeks]

- Introduce the forces present in a mechanical system
 - Distributed
 - Concentrated
- Express the virtual work produced by each of these forces
- Apply principle of virtual work and obtain the EOM
- Eliminate the reaction forces from the expression of the virtual work
- Obtain the constrained EOM (Newton-Euler form)
- Express the reaction (constraint) forces from the Lagrange multipliers



Types of Forces & Torques Acting on a Body



- Type 1: Distributed over the volume of a body
 - Inertia forces
 - Distributed forces
 - Internal interaction forces
- Type 2: Concentrated at a point
 - Action (or applied, or external) forces and torques
 - Reaction (or constraint) forces and torques



Virtual Work: Dealing with Inertia Forces

- Framework: we are considering a point P of body i. This point is associated with an infinitesimal mass element $dm_i(P)$
- Expression of the force:

 $-\ddot{\mathbf{r}}_i^P dm_i(P)$

• Virtual work produced:

$$[\delta \mathbf{r}_i^P]^T \cdot [-\ddot{\mathbf{r}}_i^P \ dm_i(P)]$$

- Comments:
 - The total virtual work produced by this type of force is obtained by summing over all points of body i:

$$\int_{m_i} -[\delta \mathbf{r}_i^P]^T \cdot \ddot{\mathbf{r}}_i^P \, dm_i(P)$$
²⁰



Virtual Work: Dealing with Mass-Distributed Forces

- Framework: we are considering a point P of body i. This point is associated with an infinitesimal mass element $dm_i(P)$. A force per unit mass, $\mathbf{f}_i(P)$, is assumed to act at point P.
- Expression of the force:

 $\mathbf{f}_i(P) dm_i(P)$

• Virtual work produced:

 $[\delta \mathbf{r}_i^P]^T \cdot \mathbf{f}_i(P) \ dm_i(P)$

- Comments:
 - The total virtual work produced by this type of force is obtained by summing over all points of body i:

$$\int_{m_i} [\delta \mathbf{r}_i^P]^T \cdot \mathbf{f}_i(P) \ dm_i(P)$$

- This type of force is rarely seen in classical multibody dynamics. Exception: the force due to the gravitational field, which leads to the weight of the body. In this case $\mathbf{f}_i(P) = \mathbf{g}$, where \mathbf{g} is the gravitational acceleration of magnitude $g \approx 9.81 \frac{m}{s^2}$ (in Madison, WI).

